NOTES

Fischer–Tropsch Synthesis over Supported Molybdenum Hexacarbonyl

During the last 5 years there has been growing interest in new types of catalysts derived from transition metal complexes with special interest focused on carbonyl complexes (1-5). Simultaneously there has been much research directed to the possible application of these materials to commercially important reactions, particularly more selective catalysts for Fischer-Tropsch synthesis (FTS) (5-10). An early report (11) showed that $Mo(CO)_6$ had no homogeneous activity for methanation or even olefin hydrogenation, an easily catalyzed reaction. However, it was later shown that when supported $Mo(CO)_6$ could be activated to yield substantially higher activity for these reactions than traditional catalysts (prepared by the reduction of a supported salt) of MoO_3 (12-16). This note reports the first study of Mo(CO)₆/Al₂O₃ under conditions conducive to FTS and demonstrates the improved activity and selectivity of this catalyst relative to MoO₃.

If present, K^+ was added to the alumina (Conoco γ -Al₂O₃, Type Catapal SB) as KNO₃ using the incipient wetness technique and the alumina was then dried at 120°C prior to calcination at 500°C (this "standard" alumina is about 28% hydroxylated, $\bar{S} = 203 \text{ m}^2/\text{g}$). "Dehydroxylated" alumina (about 0.6% residual surface OH, \bar{S} = $125 \text{ m}^2/\text{g}$) was prepared by treating standard alumina at 1000°C for 1 h (this converts much of the γ -Al₂O₃ to δ -Al₂O₃ (17)). Supported Mo(CO)₆ was prepared using the dry mixing (and rigorously air free) technique previously described (18). Following fixing the complex on the alumina by decomposition to Mo(CO)₃(ads) at 100°C in He (19), the catalyst was activated in H_2 at 500°C.

Traditional MoO₃/Al₂O₃ was prepared from $(NH_4)_2MoO_4$ using the incipient wetness technique and reduced at 500°C in flowing H₂.

Reaction was carried out in a stainlesssteel tubular reactor holding 0.7–1.0 g catalyst in a flow system. The catalyst was either activated in situ or prepared in a fused quartz reactor and then transferred to the stainless-steel reactor without exposure to air. Flows were controlled by a Brooks mass flow controller and pressure regulated by a Grove Mity-Mite back-pressure regulator. He and CO were purified with an Oxisorb cartridge (Scientific Gas Products) and the H_2 was purified with a catalytic "oxygen removing purifier" followed by 13× molecular sieves (Matheson). Reaction products were analyzed by GC using several columns and peaks were integrated with a Hewlett-Packard Model 3388A digital integrator. Details of the experimental system will be published separately.

Table 1 shows the activities of both traditional and carbonyl-derived catalysts for FTS. The *formal* turnover frequency,¹ molecules reacting per unit time per metal atom in the catalyst (regardless of the dispersion), for Mo(CO)₆/dehydroxylated alumina with 4% K⁺ is 2×10^{-2} s⁻¹. K⁺ lowers the

¹ Formal turnover frequency is related to turnover frequency by the expression $N_f = N(D)$, where D is the fractional dispersion of a catalyst. N_f is a useful parameter for comparing activities when either dispersions are unknown or chemisorption appears to yield erroneous values. CO chemisorption at 22°C and 150 Torr on a catalyst of the type used in Table 2 and then cleaned in H₂ at 500°C yielded a fractional dispersion of 0.005. Other data suggest that CO chemisorption significantly underestimates the true dispersion of these catalysts.

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Catalyst	Loading (% Mo)	% Con	version	Relative rate constant ^a		
		No K ⁺	4% K+	No K+	4% K+	
MoO ₃ /standard alumina	5	28	17	1.00	1.00	
Mo(CO) ₆ /standard alumina	4	51	56	2.7	5.5	
Mo(CO) ₆ /dehydroxylated alumina	3	66	64	5.4	9.2	

Activities of Mo Catalysts for FTS

Note. Reaction conditions: 350°C, 355 psi, 1300 h⁻¹ GHSV, $H_2/CO = 1$.

^a Values of first-order rate constant relative to the value for MoO₃/standard alumina.

activity of the traditional catalyst significantly more than for the carbonyl catalysts. Above 4% K⁺ the activity of carbonyl catalysts drops slowly, being one-half as active with 15% K⁺.

Although the exact product distribution is somewhat dependent on the reaction conditions, a typical result is shown in Table 2. These catalysts yield close to 50 atom% of the product carbon as CO₂, indicating equilibration of the water gas shift reaction. Thus, almost all of the oxygen in products leaves the reactor as CO₂ rather than H₂O. For this reason the product distribution (carbon atom% selectivity) is given on a CO_2 -free basis. The C1 through C4 products obey Anderson kinetics (20) with a probability of polymerization of 0.37, but the C5 yield is somewhat less than predicted. In the absence of K⁺ the olefin yield is greatly reduced and higher levels of K⁺ modestly increase the olefin yield.

In most cases neither the conversion nor product distribution changes significantly during 20 h of reaction. Over the temperature range 300-425°C the activation energy is 18 kcal/mol and there is a negligible change in the product distribution. From 115 to 765 psi (1 psi = 6.9×10^3 N m⁻²) the reaction is close to first-order in total pressure and the yield of CH₄ and LPG's (C2 through C4 hydrocarbons) drops slightly with increasing pressure.

The Bureau of Mines earlier studied FTS over a variety of Mo catalysts (21). Typical of the more active catalysts is No. L6117 consisting of 11% Mo/Al₂O₃ which gave a conversion of 54% at 355°C, 309 psi, 292 h⁻¹ GHSV, and $H_2/CO = 1$ corresponding to a formal turnover frequency of about 1 \times 10^{-3} s⁻¹ (or about 2 × 10^{-4} s⁻¹ at the conditions of Table 1). The products were 68% CH₄, 22% C2, and 10% C3 + C4. It is clear that the carbonyl catalyst is both significantly more active and results in less CH₄. Murchison has recently reported improved Mo catalysts for synthesizing LPG's (22). A preferred catalyst used Saran carbon (with K^+) as a support which aided in completely reducing the Mo during catalyst activation at 500°C in H_2 . This catalyst yielded 62% LPG's with a formal turnover frequency of about $1 \times 10^{-3} \text{ s}^{-1}$ at 400°C, 900 psi, 300 GHSV, and $H_2/CO = 1$ (or

TABLE 2

Product Distribution of Mo(CO)₆/dehydroxylated Alumina (4% K⁺) for FTS

Conversion (%)	CH₄	C_2H_4	C ₂ H ₆	C ₃ H ₆	C ₃ H ₈	C₄H ₈	C ₄ H ₁₀	C5	C_6^+	LPG's
64	41.1	2.1	25.6	3.0	15.3	2.9	6.2	2.3	1.6	55

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Note. Reaction conditions: as in Table 1.

about $3 \times 10^{-5} \text{ s}^{-1}$ at the conditions of Table 1). After 500 h on stream XPS analysis showed that 53% of the Mo remained zero valent.

We suggest that the high activity of Mo(CO)₆/dehydroxylated alumina is mainly due to the ability to initially prepare the Mo in an oxidation state close to zero. Reduction of MoO₃/alumina at 500°C yields primarily Mo^{4+} (23). Activation of $Mo(CO)_6/$ standard alumina at 500°C in an inert atmosphere yields an average oxidation state of Mo⁵⁺ due to reaction of the initially zero valent Mo with surface OH groups (24). As in the case of a traditional catalyst, H_2 at 500°C reduces this material to mainly Mo⁴⁺ (19). However, this catalyst is several fold more active than the MoO₃ catalyst of this study (and much more active than the Bureau of Mines catalyst). Both the use of a zero valent catalyst precursor and the use of dehydroxylated alumina appear important in achieving maximal activity (25, 26). The exact oxidation state of the Mo during reaction is uncertain. Some oxidation of Mo(O) must occur since Mo(CO)₆/dehydroxylated alumina is only modestly more active than Mo(CO)₆/standard alumina. However, after 20 h of reaction at a conversion of 65% about 1500 molecules of water have been formed per Mo atom, but the catalyst still retains good activity. Thus, it appears that once synthesized in a low valent state the catalyst is at least modestly resistant to reoxidation to Mo^{4+} and Mo^{6+} , as also found by Murchison for Mo/C (22).

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Received January 12, 1983

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