Single step catalytic production of diisopropyl ether (DIPE) from acetone feedstock over nickel based catalysts

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Abstract

Single step production of DIPE as oxygenates from acetone feed stock was evaluated by employing Ni–Cu and Ni–Cu–Cr supported on H-zeolite-β catalysts. The influence of experimental parameters like effect of amount of catalyst loading, hydrogen pressure, reduction temperature of the precursor, volume of acetone and temperature on DIPE production is studied. Ni–Cu (25 wt.%) metal supported on H-zeolite-β catalyst shows higher activity. The dependence of the yield of DIPE on the other loadings has also been studied. The reduction temperature of the catalyst precursor is found to be less significant above 573 K. A moderate reaction temperature in the range of 433–453 K and hydrogen pressure (30–80 bar) favor the higher yield of DIPE. Ni–Cu–Cr/H-zeolite-β is also found to be active for the production of DIPE from acetone.
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1. Introduction

Oxygenates are an important class of compounds used as blending components to improve the combustion efficiency of gasoline pool. Blending of oxygenates with the gasoline results in increased combustion, thereby reducing the CO and hydrocarbon (HC) emission to a large extent under full load operating conditions [1]. The three primary functions of the oxygenates in blended gasoline are extending the gasoline pool, boosting the octane values and providing refiner with additional blending flexibility to meet ever increasing product demands [2]. Several oxygen containing compounds such as alcohols and tertiary ethers have been explored to increase the performance of gasoline. Alcohols such as ethanol and methanol were recognized as octane boosters in 1920. But the usage of alcohols as oxygenates is limited due to their higher solubility in water and unfavorable vapor pressure [3]. Tertiary alkyl ether based oxygenates such as methyl tertiary butyl ether (MTBE), ethyl tertiary butyl ether (ETBE), tertiary amyl ethyl ether (TAEE), tertiary amyl methyl ether (TAME), isopropyl tertiary butyl ether (IPTBE) and diisopropyl ether

(DIPE) are the other possible compounds for gasoline blending [4]. The physical and blending properties of tertiary ethers have been investigated extensively [5]. MTBE was employed as oxygenates in gasoline pool to improve the combustion in many countries, but the predominant usage of MTBE was restricted due its high solubility in water and its toxic nature [6,7]. In recent years, there is a growing interest in the production of DIPE as a possible oxygenate for gasoline blending. Favorable blending properties, ready availability of feedstocks and lower solubility of DIPE in water of make it an efficient alternative to MTBE [8]. Catalytic production of DIPE from propylene feed stock is a widely used process for DIPE production in petroleum refinery. Several types of acidic catalysts such as heteropoly acids [9], ion exchange resins [10], nafion [11], clays and zeolites have been employed as catalysts for DIPE production. Zeolites were exploited extensively compared to other solid acid catalysts due to their uniform pore size, high thermal stability and desired product selectivity. H-ZSM-5, H-ZSM-12, H-ZSM-35, H-zeolite-β, H-zeolite-Y and H-mordenite [12–14] are examples of zeolites, which are utilized for the production of DIPE. Apart from propylene feedstock, crude acetone, which is obtained as a byproduct in propylene oxide industry is used as an alternate feedstock for the preparation of DIPE. This alternative route is extensively studied using bifunctional

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catalysts under high-pressure vapor phase conditions [15]. The process involves hydrogenation of acetone to isopropanol followed by etherification to DIPE in a single or two-step process. Supported bimetallic systems such as Ni–Cu/alumina, Ni–Cu/H-zeolite-β, Ni–Cu/H-ZSM-5, PW/SiO$_2$ and Pd/H-zeolite-β are various catalysts employed for this process [16]. Different types of reactors such as two and three zone reactors have been utilized for the single step production of DIPE from acetone [17,18]. Supported multi-metallic systems such as Fe–Cr–Mn/H-zeolite-β, Ni–Cu/H-zeolite-β (zone-I; hydrogenation) and dealuminated H-zeolite-Y (zone-II; etherification) were used as catalysts to evaluate the effect of temperature on the DIPE formation [19].

In this paper, the catalytic activity of Ni–Cu and Ni–Cu–Cr multi-metallic catalysts supported on H-zeolite was evaluated for single step liquid phase production of DIPE from acetone feedstock. The supported metallic catalysts were characterized by XRD, EPR, SEM, EDAX and sorptometric measurements. The influence of experimental parameters such as pressure, temperature, catalyst amount and percentage loading of Ni–Cu on DIPE production was studied in detail.

2. Experimental

2.1. Catalyst preparation

2.1.1. Preparation of Ni–Cu/H-zeolite-β and Ni–Cu–Cr/H-zeolite-β

The zeolite supported bimetallic catalysts were prepared by wet impregnation method. A series of supported Ni–Cu catalysts were prepared by varying the metal loadings in the range of 5–45 wt.%. Typically, for the preparation of 25 wt.% Ni–Cu/H-zeolite-β, 42 g of nickel nitrate and 7.3 g of copper nitrate were added to an aqueous suspension of 31 g of H-zeolite-β with SiO$_2$/Al$_2$O$_3$ ratio of 40 (Ni:Cu atomic ratio 5:1). The mixture was stirred for 24 h at room temperature and heated under stirring to evaporate the water till dryness. This material was then calcined at 723 K for 8 h and reduced under hydrogen atmosphere at 623 K for 24 h prior to the catalytic studies. The 25% Ni–Cu/H-zeolite-β catalyst is also prepared by using H-zeolite-β with ratio of SiO$_2$/Al$_2$O$_3$ = 30 as support to study the effect of pressure and temperature. The Ni–Cu–Cr/H-zeolite-β catalyst was prepared using similar procedure as described. Typically, 23 g of nickel nitrate, 13.3 g of copper nitrate and 4.5 g of chromium nitrate were added to 50 g of H-zeolite-β (SiO$_2$/Al$_2$O$_3$ ratio 30) in water. The solution was stirred for 24 h at room temperature and heated to dryness under constant stirring. The catalyst was calcined at 723 K for 8 h and reduced at 623 K for 24 h prior to the catalytic studies.

2.1.2. Catalyst characterization

The powder X-ray diffraction patterns of the samples were recorded using Shimadzu XD-D1 X-ray diffractometer using Ni-filtered Cu Kα radiation (λ = 1.5418 Å). The X-band EPR spectra were recorded at liquid nitrogen temperature with a Varian E112 EPR spectrometer. Magnetic field was modulated at 100 kHz and the g-values were determined by measuring the magnetic field H and the microwave frequency in comparison with DPPH (2,2′-diphenyl-1-picrylhydrazyl) standard (g = 2.0036). The prepared catalysts were analyzed by EDAX and SEM using JEOL, JSM5610LV.

2.2. Catalytic activity

The catalytic activity for transformation of acetone to diisopropyl ether was studied under hydrogen atmosphere in the temperature range 393–453 K and pressure range of 20–80 bar using a Parr reactor (Parr Instrument Company, USA, model no. 4842). All the catalysts were reduced at 623 K for 24 h prior to the catalytic experiments and carefully transferred to the reactor vessel. Typically, 2.5 g of the catalyst was added to 40 ml acetone and placed in the reactor. The reactor was then brought to the required pressure and temperature and maintained at constant stirring. Small amount of the reaction mixtures were removed periodically and analyzed by gas chromatography (AIMIL-Nucon 5765, India). The reaction mixture was analyzed under isothermal mode (323 K) using a flame ionization detector and carbowax 20 m column.

3. Results and discussion

3.1. X-ray diffraction patterns of catalyst precursors

The XRD pattern of the H-zeolite-β exhibits two intense reflections at d-values of 11.4 and 3.99 Å as presented in Fig. 1a. These values agree with those reported in literature and indicate crystalline nature [20]. Fig. 1b–f depicts the XRD patterns of nickel based bimetallic and trimetallic catalysts supported on H-zeolite-β. In addition to the peak of parent
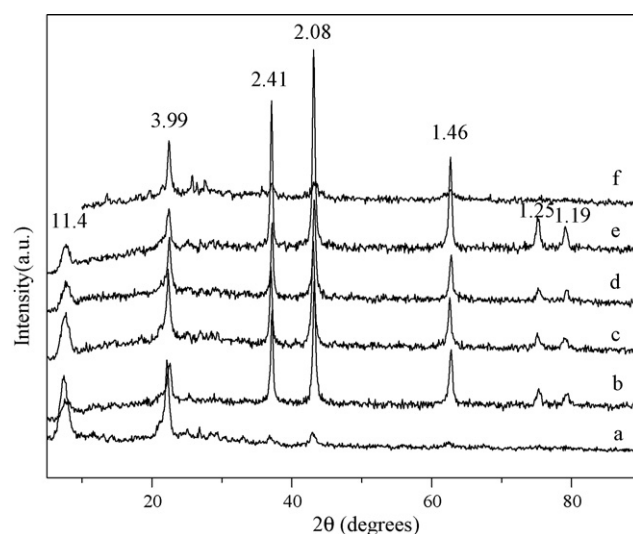

Fig. 1. X-ray diffraction patterns of the supported metallic systems with various loading of Ni–Cu on H-zeolite-β (SiO$_2$/Al$_2$O$_3$ = 40): (a) 5 wt.% Ni–Cu/H-zeolite-β, (b) 15 wt.% Ni–Cu/H-zeolite-β, (c) 25 wt.% Ni–Cu/H-zeolite-β (d) 35 wt.% Ni–Cu/H-zeolite-β, (e) 45 wt.% Ni–Cu/H-zeolite-β, and (f) 15 wt.% Ni–Cu–Cr/H-zeolite-β (SiO$_2$/Al$_2$O$_3$ = 40).

zeolite, additional peaks were observed at *d*-values of 2.41, 2.08, 1.46, 1.25, and 1.19 Å. These *d*-values correspond to the reflections from the (2 0 0), (1 1 1), (2 2 0), (3 1 1) and (2 2 2) planes of the supported NiO and (Ni, Cu) O phases (47-1949 and 25-1049). The X-ray reflections of pure CuO were not observed because of lower amount of Cu loading with respect to Ni. Similarly, the reflections of pure chromium oxides were not observed in case of trimetallic systems. The existence of the zeolite peaks at 11.4 and 4.0 Å in the supported metallic catalyst indicates that the crystalline nature of the zeolite is retained in the catalyst.

3.2. ESR spectroscopic study

Electron spin resonance spectroscopic study was carried out to obtain information on the presence and chemical state of copper in the Ni–Cu/H-zeolite-β catalyst precursors. The ESR spectra of the catalysts are shown in Fig. 2. The
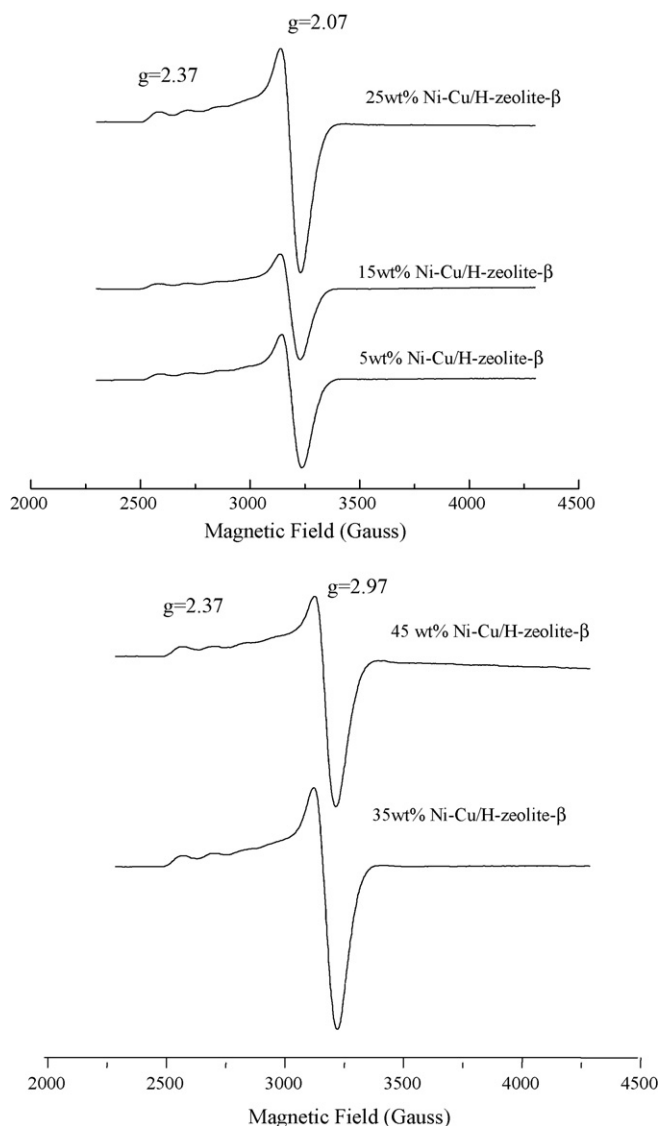

Fig. 2. ESR spectra of the supported metallic systems with various loading (5–45 wt.%) of Ni–Cu on H-zeolite-β (SiO$_2$/Al$_2$O$_3$ = 40).

signal observed at higher magnetic field corresponds to a $g_\perp$ value of 2.07, while hyperfine splitting pattern of Cu^{2+} ($I = 3/2$) was observed at lower magnetic field with a $g_\parallel$ value of 2.37. These values are typical of CuO particles and have been observed for well dispersed supported systems [21].

4. Surface area and SEM analysis

Nitrogen adsorption studies were carried out to measure the surface area and pore volumes of the catalyst precursors. The surface area and pore volume of the Ni–Cu and Ni–Cu–Cr metals supported on H-zeolite-β are given in Table 1. It has been observed that with an increase in the metal loading on H-zeolite-β catalyst, the surface area and pore volume were found to decrease. This is due to the partial blocking of the pores in the zeolite matrix by the supported metallic particles. The 45 wt.% Ni–Cu supported on H-zeolite-β show minimum pore volume and surface area. The surface compositions of the bimetallic particles as determined by EDAX analysis are also presented in Table 1.

In general, a good agreement was observed between the amount of metal used and the data obtained from EDAX analysis. However, the Ni to Cu ratio is found to be different form the original value of 5:1. This is ascribed to the lower surface energy of copper (1850 mJ m^{-2}) compared to nickel (2450 mJ m^{-2}) which results in surface segregation of copper metal on the surface of the Ni–Cu particles. Scanning electron microscopic pictures were taken to study the morphology of the catalysts. The SEM pictures of the supported metal systems are shown in Fig. 3. The supported catalyst particles are of irregular shape and are non-homogeneous. The surfaces of the supported metal catalysts are generally rough without growth of small particles. The surface morphology of the catalyst is little affected by the variation in the amount of metal loading.

4.1. Effect of amount of (Ni–Cu) loading on H-zeolite-β for the production of DIPE

The effect of amount of metal loading on the yield of DIPE for a series of catalysts in the range of 5–45 wt.% was studied and the results are presented in Table 2. The DIPE yield is

Table 1
Surface area, pore volume and atomic percent (Ni and Cu) data for Ni–Cu/H-zeolite-β catalyst

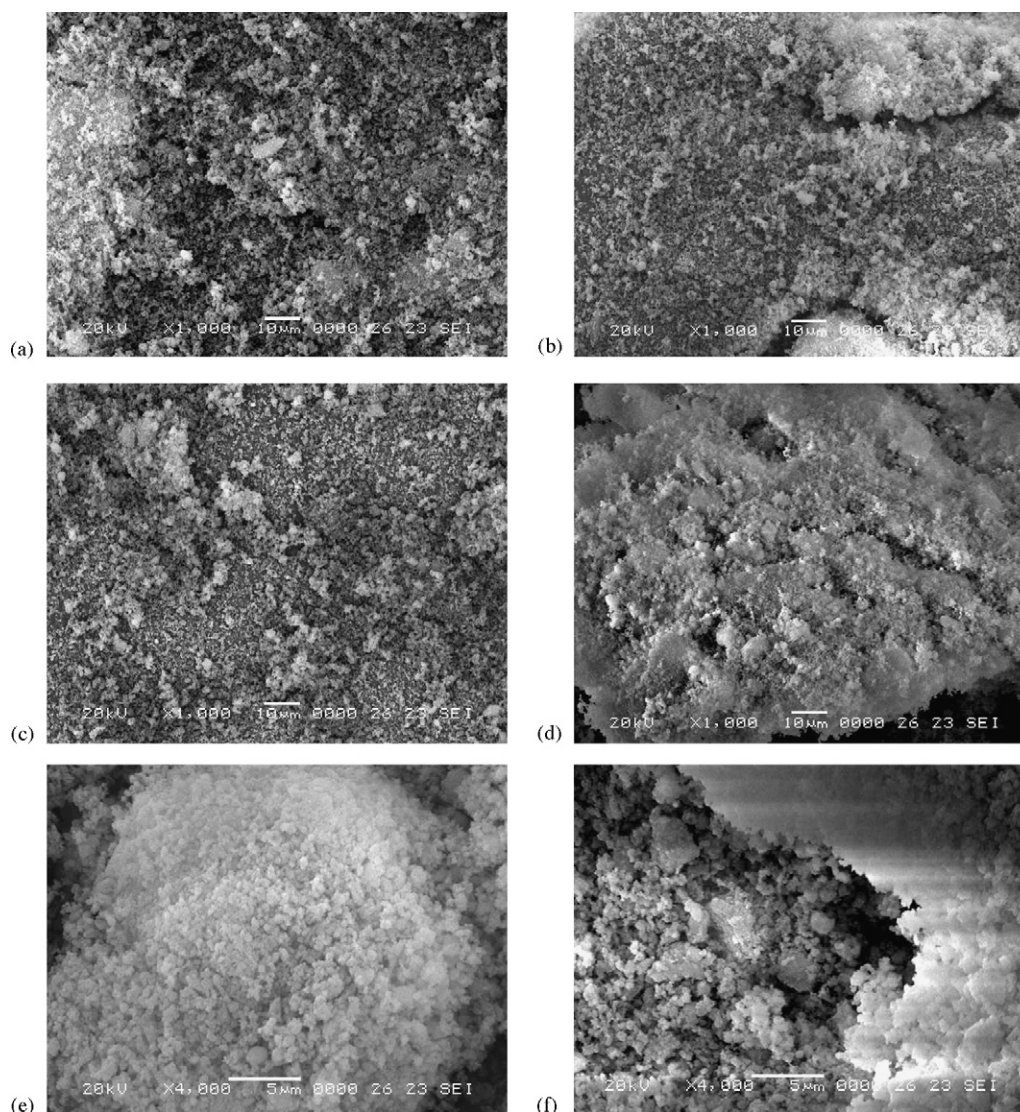| Catalyst	Pore volume (cm^3/g)	Surface area (m^2/g)	Atomic percent[a]	
			Ni	Cu
H-zeolite-β	0.47	406	–	–
5 wt.% Ni–Cu/H-zeolite-β	–	–	2.56	2.33
25 wt.% Ni–Cu/H-zeolite-β	0.43	347	18.8	8.6
35 wt.% Ni–Cu/H-zeolite-β	0.38	257	24.7	7.2
45 wt.% Ni–Cu/H-zeolite-β	0.30	241	33.8	9.5
15 wt.% Ni–Cu–Cr/H-zeolite-β	0.33	315	–	–

[a] Data obtained from EDAX analysis.

Fig. 3. SEM picture of: (a) H-zeolite-β, (b) 15 wt.% Ni–Cu/H-zeolite-β, (c) 25 wt.% Ni–Cu/H-zeolite-β, (d) 35 wt.% Ni–Cu/H-zeolite-β, (e) 15 wt.% Ni–Cu–Cr/H-zeolite-β, and (f) 25 wt.% Ni–Cu–Cr/H-zeolite-β.

found to increase with an increase in the metal loading up to 25 wt.% and further increase in loading leads to decrease in DIPE yield. The optimum metal loading was found to be 25 wt.% for the maximum yield of DIPE. It has been observed that a considerable amount of MIBK was formed with 5 wt.% Ni–Cu/H-zeolite-β catalyst.

Table 2
Effect of amount of metal loading on the activity and DIPE yield on Ni–Cu/H-zeolite-β catalyst ($SiO_2/Al_2O_3 = 40$)

Catalyst	Conversion (wt.%)	Product composition (mol%)		
		DIPE	IPA	MIBK
5 wt.% Ni–Cu/H-zeolite-β	78.2	6.0	36.0	18.3
15 wt.% Ni–Cu/H-zeolite-β	99.6	11.0	78.0	–
25 wt.% Ni–Cu/H-zeolite-β	99.3	30.5	45.2	–
35 wt.% Ni–Cu/H-zeolite-β	98.0	26.1	51.3	–
45 wt.% Ni–Cu/H-zeolite-β	96.4	24.5	52.4	–

4.2. Effect of Ni:Cu ratio on H-zeolite-β on the production of DIPE

Catalytic activity of 25 wt.% Ni/H-zeolite-β, 25 wt.% Ni–Cu (3:1)/H-zeolite-β and 25 wt.% Ni–Cu (5:1)/H-zeolite-β was studied for the production of DIPE from acetone at 433 K and a pressure of 60 bar for a time period of 5 h to evaluate the role of copper on the DIPE yield (Table 3). Isopropanol and DIPE are the products obtained on all the catalysts. Isoproanol formation is more in the case of Ni/H-zeolite-β and Ni–Cu (3:1)/H-zeolite-β. However, on 25 wt.% Ni–Cu (5:1)/H-zeolite-β the catalyzed

Table 3
Effect of Ni:Cu ratio on H-zeolite-β on the production of DIPE

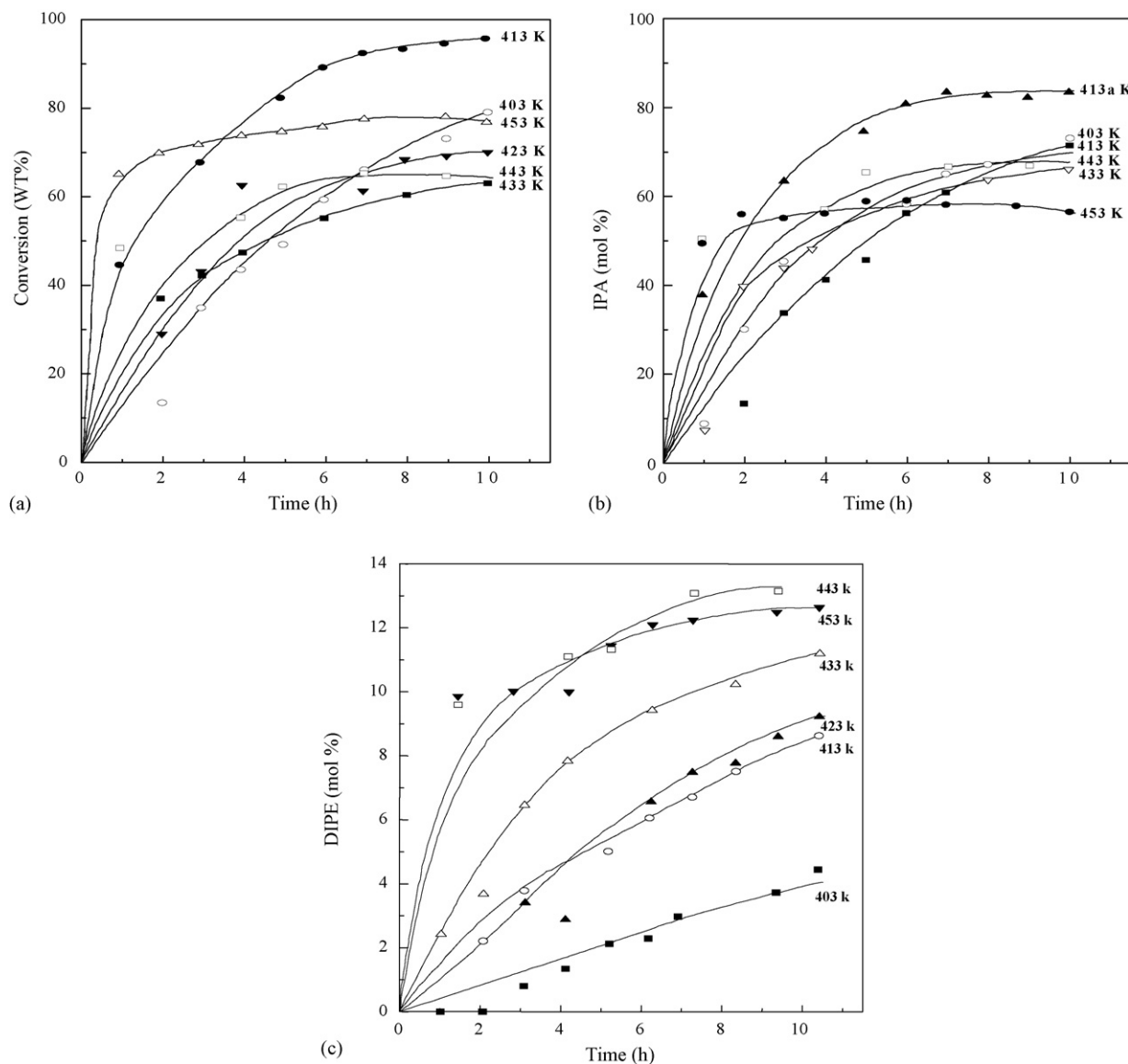| Catalyst	DIPE (mol%)	IPA (mol%)
25 wt.% Ni/H-zeolite-β	22.2	52.3
25 wt.% Ni–Cu (3:1)/H-zeolite-β	24.8	52.0
25 wt.% Ni–Cu (5:1)/H-zeolite-β	30.5	45.2

Fig. 4. Effect of temperature on the catalytic activity of 25 wt.% Ni–Cu/H-zeolite-β catalysts at 60 bar on: (a) acetone conversion, (b) IPA yield, and (c) DIPE yield.

reaction results in the formation of higher amount of DIPE compared to other two catalysts.

4.3. Effect of reduction temperature on catalytic activity of 25 wt.% Ni–Cu/H-zeolite-β catalyst (SiO₂/Al₂O₃ = 40)

The catalyst precursors (oxide form) were reduced in an atmosphere of hydrogen at higher temperature to generate the active metallic supported catalyst. The effect of the reduction temperature on catalytic activity was studied for the 25 wt.% Ni–Cu/H-zeolite-β catalyst by varying the reduction temperature of the catalyst precursor in the temperature range of 573–773 K. The reduction temperature has little effect on the activity of the catalyst in the range of temperature studied as given in Table 4 and the DIPE yield is also found to remain unchanged in this temperature range. This indicates that the reduction of the oxide precursor to the corresponding metal is accomplished at 573 K and facilitates DIPE formation.

4.4. Influence of reaction temperature on the catalytic activity of 25 wt.% Ni–Cu/H-zeolite-β catalyst (SiO₂/Al₂O₃ = 40)

The catalytic activity of 25 wt.% Ni–Cu/H-zeolite-β for DIPE production was evaluated at different temperatures (403–453 K)

Table 4
Effect of reduction temperature on the activity and DIPE yield on 25 wt.% Ni–Cu/H-zeolite-β catalyst (SiO₂/Al₂O₃ = 40)

Reduction temperature (K)	Conversion (wt.%)	Product composition (mol%)	
		DIPE	IPA
573	100.0	28.7	48.9
623	96.0	27.8	46.7
673	100.0	30.2	46.4
723	94.2	28.2	44.2
773	97.9	29.1	46.0

Table 5
Effect of hydrogen pressure on DIPE and IPA yield over 25 wt.% Ni–Cu/H-zeolite-β catalyst

Pressure (bar)	Conversion (wt.%)	Product composition (mol%)	
		DIPE	IPA
20	77.0	16.9	47.0
40	98.3	26.2	51.4
60	100	30.4	46.1
80	99.9	30.7	45.5

for a reaction time period of 10 h (Fig. 4). Acetone conversion was found to increase with reaction time and attain a saturation value around 5–7 h in the temperature range studied (Fig. 4a). Isopropanol and DIPE were obtained as major products along with minor amount of methyl isobutyl ketone. The effect of temperature on the yield of isopropanol and DIPE in the range of 403–453 K is shown in Fig. 4b and c. High reaction temperature conditions favor DIPE formation while isopropanol is formed as a major product under low reaction temperatures. At low temperatures (403–423 K) the hydrogenation of acetone is favored leading to the formation of isopropanol. However, the subsequent bimolecular dehydration of isopropanol to DIPE is not efficient. On the other hand, DIPE yield increases in the temperature range of 433–453 K indicating that the acidic sites of the H-zeolite-β is active towards etherification at higher temperatures.

4.5. Ni–Cu/H-zeolite-β catalyst (SiO₂/Al₂O₃ = 40)

Liquid phase production of DIPE over zeolite supported metallic catalysts was generally carried out in the atmosphere of hydrogen. The effect of pressure of hydrogen on the DIPE yield with 25 wt.% Ni–Cu/H-zeolite-β is studied in the range of 20–80 bar at 433 K and the results are given in Table 5. It is observed that the DIPE yield increases with increase in pressure before it attains a constant value around 60 bar.

4.6. Catalytic activity of 35% Ni–Cu/H-zeolite-β for DIPE production

Under identical reaction conditions, 35 wt.% loading of Ni–Cu on H-zeolite-β produces higher yield of DIPE (26.1%) next to 25% Ni–Cu/H-zeolite-β (30.5%). Catalytic activity of 35% Ni–Cu/H-zeolite-β for the preparation of DIPE from acetone at 60 bar was studied in the range of 393–443 K in order to evaluate the influence of temperature on the catalytic activity. The acetone conversion, IPA and DIPE yield at different reaction temperatures are shown in Fig. 5. The data show the variation in the yield of DIPE at various temperatures studied (393–443 K). The temperature response of 35 wt.% Ni–Cu/H-zeolite-β is found to be identical to that of 25 wt.% Ni–Cu/H-zeolite-β and agrees with those reported in literature where the yield of DIPE increases with increase in temperature [20].
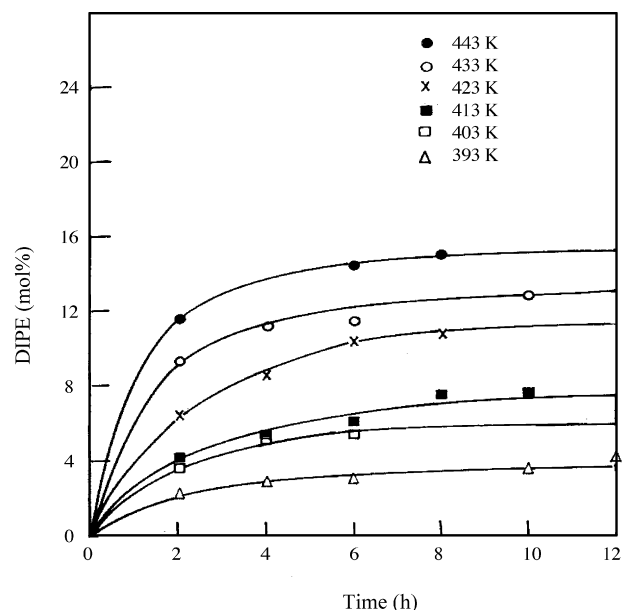

Fig. 5. Effect of temperature on the catalytic activity of 35 wt.% Ni–Cu/H-zeolite-β (SiO₂/Al₂O₃ = 30).

4.7. Recyclability of 25 wt.% Ni–Cu (5:1)/H-zeolite-β

The recovery and reusability of 25 wt.% Ni–Cu/H-zeolite-β was studied. After the completion of the reaction, the catalyst was filtered, washed with acetone and regenerated in oxygen atmosphere at 823 K for 12 h followed by hydrogen reduction at 623 K for 24 h. The recovered catalyst was employed for further runs and the whole process was repeated for three times (Table 6). The activity of the recycled catalyst gradually decreased upon successive use possibly due to agglomeration of the metallic component by activation at higher temperatures.

4.8. Diisopropyl ether production from acetone using trimetallic Ni–Cu–Cr/H-zeolite-β catalyst

4.8.1. Effect of zeolite support on the catalytic activity of Ni–Cu–Cr/H-zeolite

Influence of the type of zeolite as supports for Ni–Cu–Cr on the production of DIPE from acetone was studied by employing

Table 6
Recyclability of 25 wt.% Ni–Cu/H-zeolite-β for acetone transformation to DIPE

Conversion (wt.%)	
Fresh	100
I cycle	88.0
II cycle	83.5
IPA (mol%)	
Fresh	45.2
I cycle	44.2
II cycle	55.0
DIPE (mol%)	
Fresh	30.5
I cycle	25.2
II cycle	16.5

Temperature = 433 K; pressure = 60 bar; time = 5 h.

Table 7
Influence of zeolite support on the catalytic activity of Ni–Cu–Cr

Catalysts	Time (h)	Acetone (wt.%)	IPA (mol%)	DIPE (mol%)	Conversion (wt.%)
Ni–Cu–Cr/H-ZSM-5	5	0.0	93.8	0.0	100
Ni–Cu–Cr/H-mordenite	5	34.0	62.1	1.3	66.0
	10	37.5	60.0	0.3	62.5
	15	47.5	50.5	0.1	52.5
Ni–Cu–Cr/H-zeolite-β	10	43.8	37.5	8.4	56.2

Temperature: 433 K; pressure: 60 bar with hydrogen; acetone volume: 40 ml.

H-ZSM-5, H-mordenite and H-zeolite-β. Transformation of acetone was studied at a temperature of 433 K and 60 bar pressure and the results obtained are given in Table 7. Catalyst system supported on HZSM-5 showed complete conversion of acetone into IPA without further transformation to DIPE. Catalyst system supported on H-mordenite afforded around 60% of IPA along with trace amount of DIPE and even though conversion of acetone over H-zeolite-β supported system was lower, it gave rise to considerable amount of DIPE (8.4 mol%) along with the formation of IPA.

4.9. Diisopropyl ether production from acetone using 15 wt.% Ni–Cu–Cr/H-zeolite-β catalyst ($SiO_2/Al_2O_3 = 30$)

The acetone hydrogenation reaction followed by its dehydration to DIPE was carried out on 15 wt.% Ni–Cu–Cr/H-zeolite-β catalyst with SiO_2/Al_2O_3 ratio of 30 in liquid phase in the temperature range of 413–453 K. The catalytic activity data generated are presented in Table 8. It has been observed that acetone conversion is found to increase with an increase in temperature up to 443 K. Further increase in the temperature results in decrease in acetone conversion. The products such as DIPE and IPA, which are obtained by acetone transformation at different temperatures were shown in Fig. 6. It can be seen from

Table 8
Effect of temperature on the catalytic activity of the 15 wt.% Ni–Cu–Cr/H-zeolite-β catalyst ($SiO_2/Al_2O_3 = 30$)

Time (h)	Conversion (wt.%)				
	413 K	423 K	433 K	443 K	453 K
2	53.4	40.0	58.7	74.8	62.3
4	62.1	54.7	62.3	68.4	60.9
6	76.4	62.2	54.3	71.7	60.0
8	76.9	–	57.6	63.2	60.0
10	71.0.	65.6	59.6	72.9	56.1
12	66.5	64.1	63.9	72.2	53.2

Fig. 6 that yield of DIPE increases in the temperature range 413–453 K, which is favorable for etherification reaction over acidic H-zeolite-β support.

4.10. Catalytic activity of 25 wt.% Ni–Cu–Cr/H-zeolite-β for the production of DIPE

The optimum loading of Ni–Cu was found to be 25 wt.% on H-zeolite-β for the DIPE production from acetone in liquid phase. Twenty-five wt.% Ni–Cu–Cr/H-zeolite-β was employed as catalyst to study the activity for DIPE formation in the
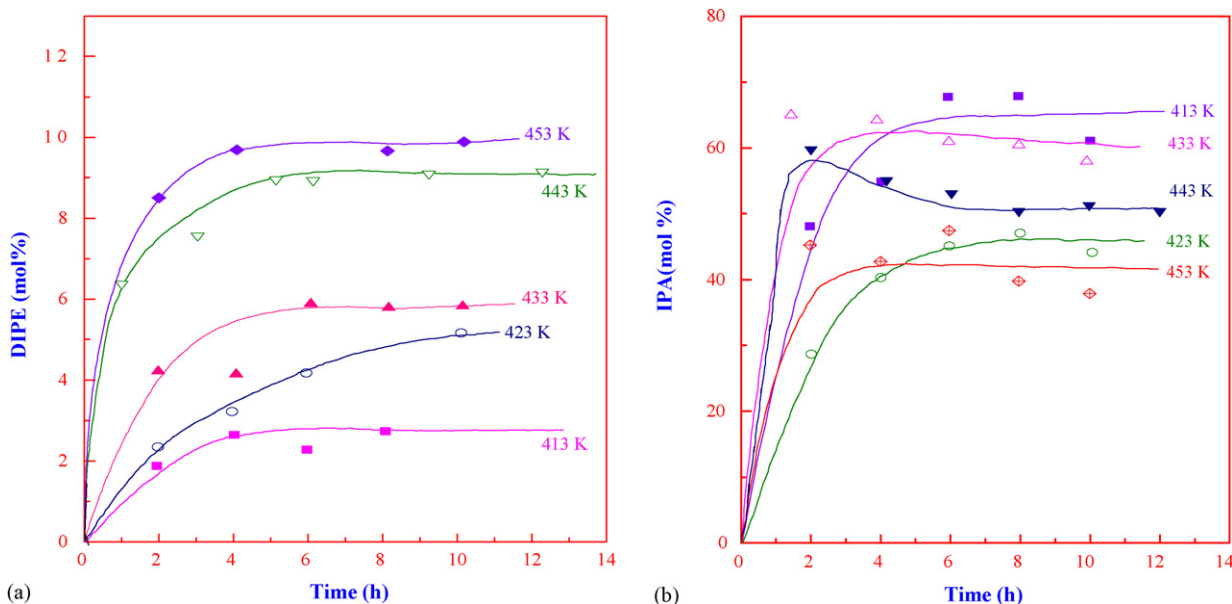

Fig. 6. Influence of temperature on the catalytic activity of the 15 wt.% Ni–Cu–Cr/H-zeolite-β catalyst ($SiO_2/Al_2O_3 = 30$): (a) DIPE yield and (b) IPA yield.

Table 9
Effect of temperature on the catalytic activity of the 25 wt.% Ni–Cu–Cr/H-zeolite-β catalyst (SiO$_2$/Al$_2$O$_3$ = 30)

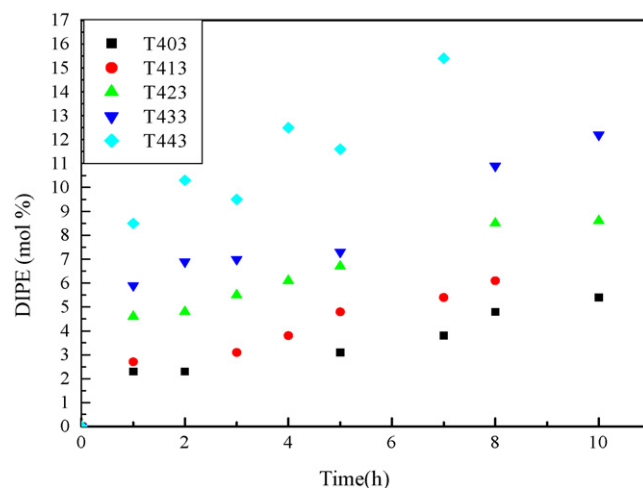| Temperature (K)	Conversion (wt.%)								IPA (mol%)								DIPE (mol%)							
	1 h	2 h	3 h	4 h	5 h	7 h	8 h	10 h	1 h	2 h	3 h	4 h	5 h	7 h	8 h	10 h	1 h	2 h	3 h	4 h	5 h	7 h	8 h	10 h
403	67.4	69.6	–	–	81.2	87.2	93.9	93.9	53.6	58.2	–	–	67.4	69.2	74.0	93.9	2.3	2.3	–	–	3.1	3.8	4.8	5.4
413	55.6	–	57.4	61.6	–	71.3	74.8	74.8	39.0	–	41.0	42.6	–	50.5	51.1	74.8	2.7	–	3.1	3.8	4.8	5.4	6.1	–
423	58.2	67.0	70.0	72.0	75.8	–	80.0	84.7	39.9	45.0	46.9	47.6	49.2	–	51.7	84.7	4.6	4.8	5.5	6.1	6.7	–	8.5	8.6
433	69.6	78.9	84.1	–	90.7	91.5	93.8	94.3	52.8	58.2	61.2	–	66.2	–	68.3	94.3	5.9	6.7	7.0	–	7.3	–	109	12.2
443	86.3	86.5	83.5	90.0	89.5	91.5	–	–	56.3	57.6	59.3	59.6	62.0	56.6.	–	–	8.5	10.3	9.5	12.5	11.6	15.4	–	–

Fig. 7. Influence of temperature on the catalytic activity of the 25 wt.% Ni–Cu–Cr/H-zeolite-β catalyst (SiO$_2$/Al$_2$O$_3$ = 30) on DIPE yield.

temperature range of 403–443 K and pressure of 60 bar. The results obtained are given in Table 9. The formation of DIPE at different time intervals and in the temperature range 403–443 K are shown in Fig. 7. It can be inferred from data in this figure that DIPE yield increases with temperature as in the case of all other catalysts studied. The temperature range (423–443 K) is appropriate for bimolecular dehydration reaction over acidic etherification catalyst namely H-zeolite-β.

4.11. Evaluation of influence of amount catalyst for the production of DIPE

In order to get information on the effect of amount of catalyst on DIPE formation, the catalyst amount was varied

Table 10
Effect of catalyst amount on acetone transformation and DIPE yield on 15 wt.% Ni–Cu–Cr/H-zeolite-β catalyst (SiO$_2$/Al$_2$O$_3$ = 30)

	Catalyst amount (g)	Time (h)				
		2	4	6	8	10
Acetone conversion (wt.%)	0.5	16.0	27.0	[a]	40.8	[a]
	1.0	52.2	69.5	79.0	84.0	87.7
	1.5	22.0	54.7	62.0	–	74.0
	2.5	–	57.0	60.5	66.5	72.7
IPA (mol%)	0.5	3.2	4.4	[a]	[a]	6.5
	1.0	43.4	56.4	61.4	64.6	67.0
	1.5	15.0	33.0	36.7	[a]	[a]
	2.5	[a]	34.0	35.9	[a]	36.2
DIPE (mol%)	0.5	[b]	[b]	[b]	[b]	[b]
	1.0	4.2	5.5	8.9	9.9	10.7
	1.5	0.7	4.2	5.0	[a]	5.2
	2.5	[a]	3.4	3.8	4.8	6.9
MIBK (mol%)	0.5	7.0	13.4	–	–	20.2
	1.0	[b]	[b]	[b]	[b]	[b]
	1.5	2.9	8.0	9.0	–	11.8
	2.5	10.2	11.6	11.8	12.5	13.7

[a] Product not collected.
[b] No product formation.

Table 11
Effect of hydrogen pressure on acetone transformation and DIPE formation on 15 wt.% Ni–Cu–Cr/H-zeolite-β catalyst (SiO$_2$/Al$_2$O$_3$ = 30), T = 423 K

Time (h)	Acetone conversion (wt.%)			IPA (mol%)			DIPE (mol%)		
	40[a]	60[a]	80[a]	40[a]	60[a]	80[a]	40[a]	60[a]	80[a]
2	40.0	82.2	87.7	29.0	69.7	72.4	2.2	5.3	6.6
4	54.7	86.8	90.7	40.0	71.4	74.4	3.3	6.3	7.1
6	62.2	91.6	97.0	45.0	75.0	76.5	4.1	7.7	10.1
8	–	92.6	97.4	–	74.8	74.8	–	8.8	11.4
10	65.6	93.0	98.0	46.0	73.0	74.7	5.3	10.0	12.0
12	64.1	93.8	98.5	41.7	63.0	60.0	7.7	14.0	20.0

[a] Pressure in bar.

Table 12
Effect of hydrogen pressure on acetone transformation and DIPE formation on 15 wt.% Ni–Cu–Cr/H-zeolite-β catalyst (SiO$_2$/Al$_2$O$_3$ = 30), T = 433 K

Time (h)	Acetone conversion (wt.%)			IPA (mol%)			DIPE (mol%)		
	30[a]	50[a]	70[a]	30[a]	50[a]	70[a]	30[a]	50[a]	70[a]
2	31.6	44.0	58.0	26.5	25.2	36.8	1.6	3.3	5.5
4	34.6	51.8	66.0	30.2	29.9	42.4	1.3	4.1	6.1
6	47.0	56.0	69.8	30.0	32.2	42.8	1.8	5.3	7.3
8	43.6	59.6	75.0	35.4	33.6	45.5	2.8	5.2	9.3
10	46.6	62.0	75.0	35.3	34.7	43.1	3.7	5.7	10.3
12	48.2	64.0	80.0	36.7	35.3	47.6	3.9	6.4	9.9

[a] Pressure is expressed in bar.

from 0.5 to 2.5 g keeping other parameters constant and the results are tabulated in Table 10. When the amount of catalyst used is 0.5 g, there is no formation of DIPE, whereas, the formation of IPA is observed during the course of the reaction. This implies that when less amount of catalyst is used, the metallic component is still promoting acetone transformation to IPA. However, amount of acidic sites are not enough to promote the etherification of IPA to DIPE. Considerable amount (5–10.7 mol%) of DIPE formation was observed when the catalyst amount is 1.0, 1.5 and 2.5 g. The DIPE yield and the selectivity

towards DIPE were found to be maximum at a catalyst loading of 1.0 g. Apart from DIPE, minimum amount of MIBK was observed in the case of 0.5, 1.5 and 2.5 g of loadings.

4.12. Effect of hydrogen pressure on the catalytic activity for the production of DIPE

The effect of hydrogen pressure on the DIPE yield is studied in the range of 40–80 bar at two different temperatures (423 and 433 K) and the results are given in Tables 11 and 12. The
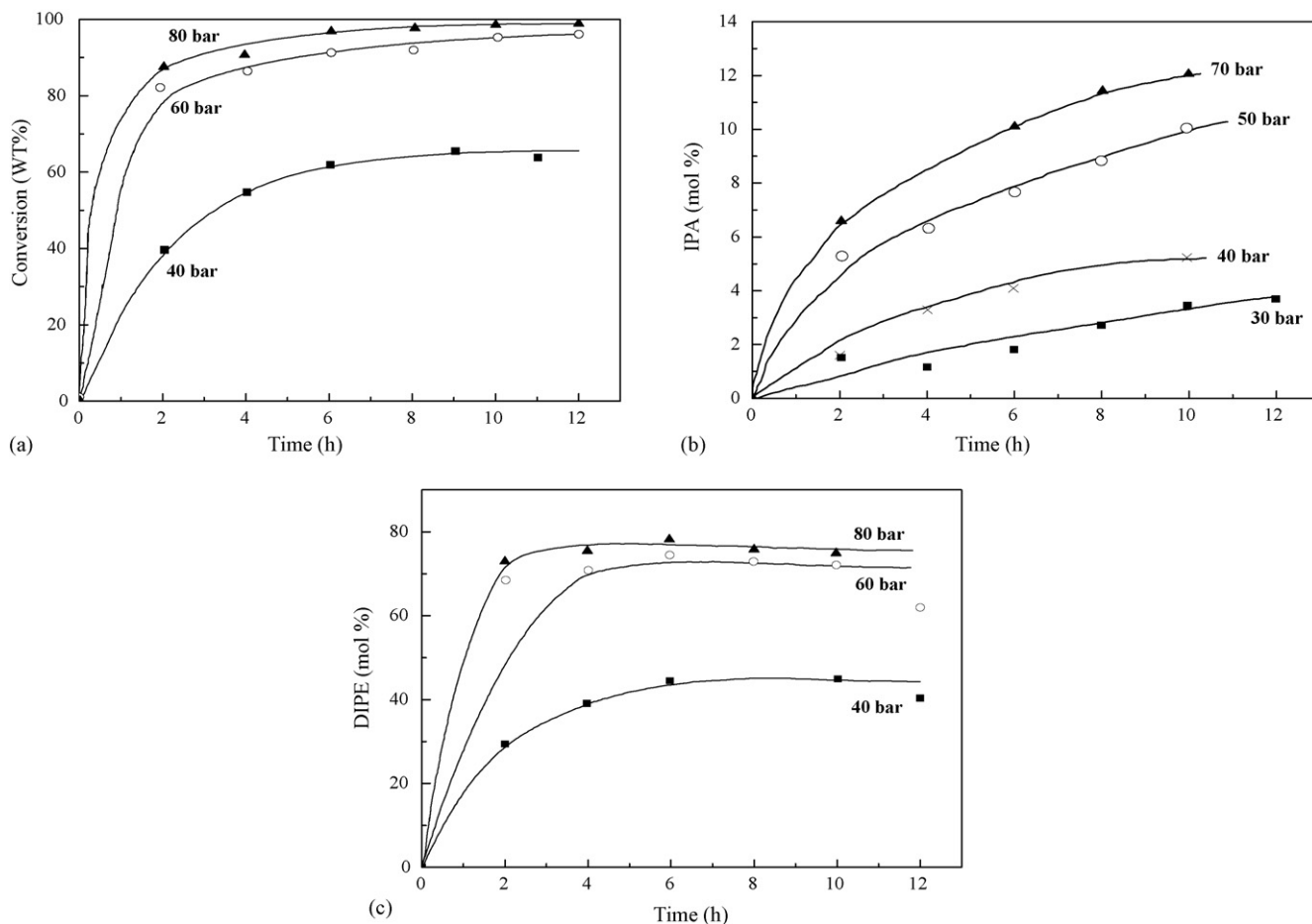

Fig. 8. Effect of hydrogen pressure on: (a) acetone transformation, and (b) IPA formation on 15 wt.% Ni–Cu–Cr/H-zeolite-β catalyst (SiO$_2$/Al$_2$O$_3$ = 30), T = 423 K. (c) DIPE formation.
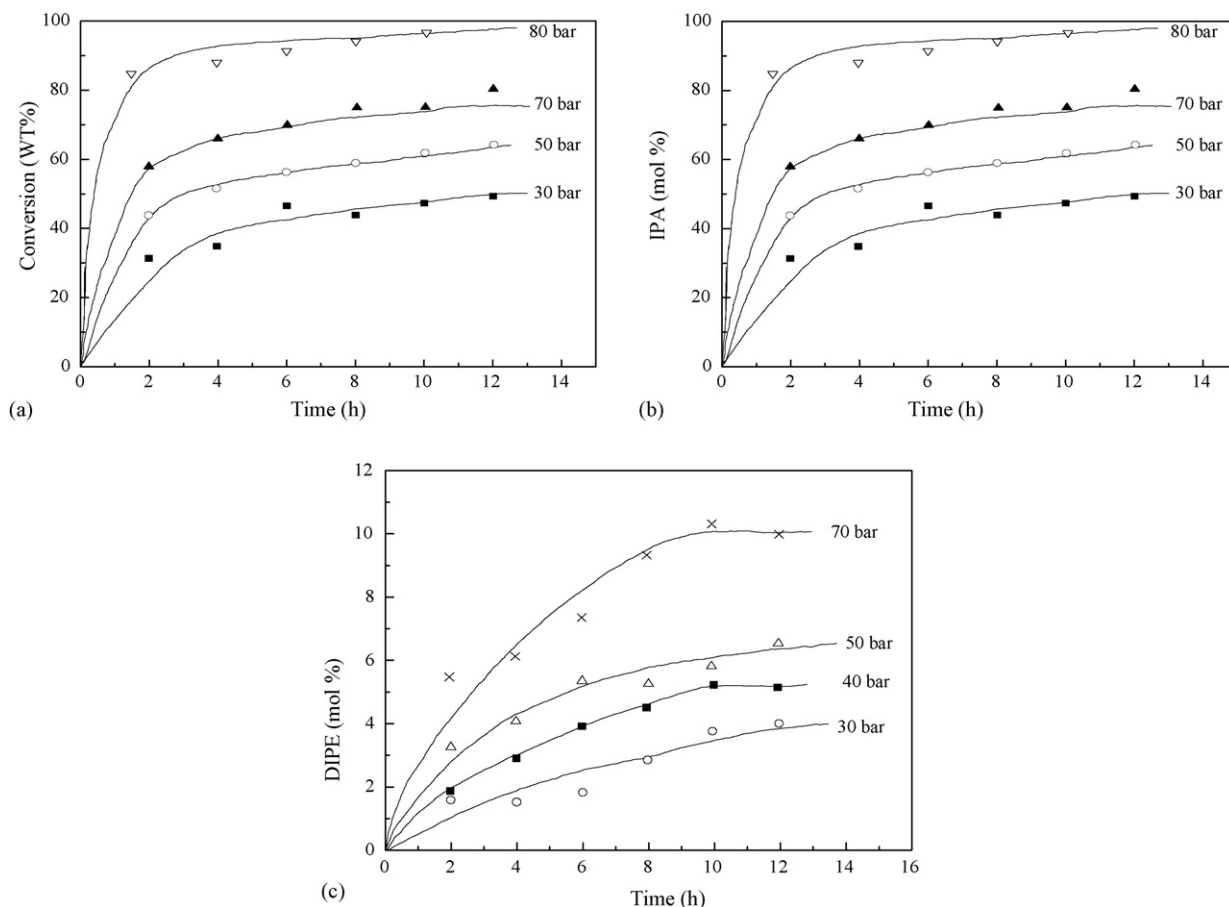
Fig. 9. Effect of pressure on: (a) acetone transformation, (b) IPA formation, and (c) DIPE formation on 15 wt.% Ni–Cu–Cr/H-zeolite-β catalyst (SiO$_2$/Al$_2$O$_3$ = 30), T = 433 K.

influence of pressure on the acetone conversion, IPA and DIPE yield are shown in Fig. 8. The DIPE yield is found to increase with increase in pressure at both temperatures. The hydrogen pressure also increased the yield of isopropanol and acetone conversion as can be seen from Fig. 9. The initial rate of reaction was calculated from the plot of DIPE yield versus time and plotted against respective hydrogen pressures. The initial rate increases linearly with pressure, which is shown in Fig. 10.

4.13. Effect of acetone concentration on the catalytic activity for the production of DIPE

The influence of acetone concentration in terms of volume on the catalytic production of DIPE was evaluated by varying the volume of acetone from 20 to 80 ml and keeping other parameters constant. The results obtained are given in Table 13 where yields of DIPE and IPA are found to decrease with increase in volume of acetone. The lowering of the activity may be due to the saturation or flooding of the catalysts surface by acetone, which results in the lower catalytic activity.

It is necessary that the results reported in this paper are considered in the light of the existing patent and open literature because of the commercial as well as some academic interest. Knifton and Dai [19] investigated this reaction employing crude acetone streams and have shown that three classes of

acidic catalysts namely H-zeolite-β modified with (Ni, Cu), (Fe–Cr–Mn) and dealuminated H-zeolite-Y promoted this reaction. They have shown that there is an increase in the ether yield (especially that of DIPE, MIPE, and DME) with an increase in the temperature range of 393–453 K. In addition they have established that the etherification is controlled by kinetic factors and the yield of the various ethers depends on the competition for the etherification sites. Their studies thus showed that the Ni–Cu on H-zeolite-β system showed more etherification sites as compared to other catalyst systems investigated by them. The results of the present study not only supports this observation but also shows that even in the pure acetone stream (that has been employed in the present work) that Ni–Cu on H-zeolite-β promotes effectively the IPA formation as well as its subsequent etherification to DIPE. In this sense, the present system is comparable to the bimetallic catalysts systems normally employed in the reforming reactions. One of the metallic components promotes the hydrogenation activity and the other metallic component not only moderates the hydrogenation activity of the first metallic component but also facilitates the etherification sites suitably. This is one aspect one has to examine in closer details in future.

Taylor and co-workers [16,17,22,23] have shown that an integrated two reactor concept either with gradient functions or use of two distinct catalyst systems with nearly 32 wt.% Ni–Cu
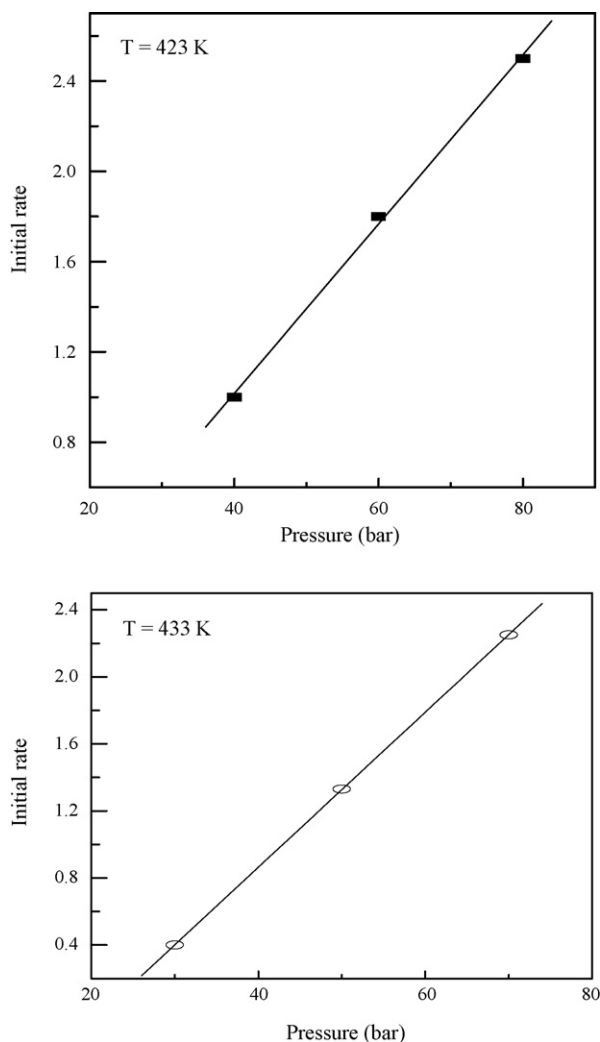
Fig. 10. Effect of hydrogen pressure on the initial rate for DIPE formation with 15 wt.% Ni–Cu–Cr/H-zeolite-β catalyst.

Table 13
Effect of acetone concentration in terms of volume on the catalytic activity of 15 wt.% Ni–Cu–Cr/H-Zeolite-β

Acetone volume (ml)	Time (h)	Conversion (wt.%)	IPA (mol%)	DIPE (mol%)
20	5	87.6	52.5	17.4
40	6	63.5	35.9	3.8
60	5	41.1	34.7	2.0
80	5	12.2	4.9	–

Pressure = 60 bar; temperature = 433 K.

The preferential segregation of copper over nickel not only modulates the hydrogenation activity of acetone to IPA but also modulates the etherification activity of the H-zeolite-β. The addition of the third element especially Cr favors hydrogenation activity over the etherification reaction and hence the choice of the third component should be based on increasing the surface acidity of the catalyst and inhibiting or reducing the hydrogenating activity. Therefore, the choice of the third component has to be found elsewhere and not in the transition metal series as has been reported in literature. The results presented in this study is based on pure acetone feed as compared to the crude acetone feed or refinery based propylene feed and in this sense the results of these studies have to be contrasted with the results reported in literature and has to be evaluated for its worth. It appears that the production of oxygenate, namely DIPE a potential gasoline blend needs a relook in the light of the results presented in this communication.

5. Conclusion

In this study, an attempt has been made towards the synthesis of DIPE from acetone in a single step under liquid phase conditions for the first time. Ni–Cu bimetallic catalysts supported on H-zeolite-β are found to be active for DIPE production. The amount of metal loading, temperature and hydrogen pressure were crucial factors for higher yields of DIPE. Twenty-five wt.% Ni–Cu metal supported on H-zeolite-β catalyst shows higher activity and DIPE yield compared to other metal loadings studied. The reduction temperature of the catalyst precursor is found to be less significant when it is higher than 573 K. Ni–Cu–Cr trimetallic catalysts supported on H-zeolite-β are also found to be active for the production of DIPE from acetone reaction. The effect of amount of catalyst loading, hydrogen pressure, volume of acetone and temperature on DIPE formation was studied. A moderate reaction temperature in the range of 433–453 K and catalyst amount of 1 g (wt.%) are found to be favorable for higher DIPE yields. Hydrogen pressure (30–80 bar) increases the yield of DIPE.

on metal zeolite–alumina gave nearly 30 wt.% of DIPE yield with least amount of undesirable gas. In the present study, the optimum catalyst composition is 25 wt.% of Ni–Cu on H-zeolite-β and the DIPE yield is also around 30 mol% which are in agreement with the results reported by Taylor et al. [23]. However, the striking difference is that the present study eliminates the two reactor concept and shows that a single catalyst system itself is capable of promoting both hydrogenation as well as etherification reaction.

In a series of patents [16,18,22,23] Texaco Chemical Inc., has shown that an integrated catalysts reactor system for the conversion of crude acetone to DIPE while in another series of patents [11,12,14] the same reaction is achieved using propylene as the feed. The present study demonstrates that one can not only eliminate the use of two reactor concept (though the chemical identity is the same, the compositions were different) but also shows a catalyst of a single composition is capable of promoting acetone to DIPE reaction effectively in consecutive fashion. The optimum composition of the single catalyst and the temperature range (403–443 K) of operation are also established for optimum conversion to the oxygenates especially DIPE.

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